

# Data Compilation for AGC-2 Matrix-only Compact Lot A3-P33

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Revision 0

November 2010

Prepared for the
United States Department of Energy Office of Nuclear Energy
under the
Next Generation Nuclear Plant –
Advanced Gas Reactor Fuel Development Program

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### Data Compilation for AGC-2 Matrix-only Compact Lot A3-P33

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This document is a compilation of fabrication and characterization data for the compact lot A3-P33, which was produced for possible insertion into the second ATR Graphite Creep irradiation test capsule (AGC-2). The compacts were produced by Oak Ridge National Laboratory (ORNL) for the Advanced Gas Reactor Fuel Development and Qualification (AGR) program. This compact lot was fabricated using a graphite/resin blend formulated by INL as a candidate matrix precursor for scale-up of overcoating and compacting processes. The matrix precursor powder for compact lot A3-P33 was a jet milled blend of 64 wt% natural graphite (Asbury 3482), 16 wt% synthetic graphite (Graftech GTI-D), and 20 wt% of a developmental novolac resin (Plenco 14433).

The "Matrix Compacts for AGC-2 Irradiation" Specification (INL SPC-1285, Rev. 1) provides the requirements necessary for acceptance of the compacts. Sections 2.03 and 2.04 of SPC-1285 provide the property requirements for the heat-treated compacts. There are requirements on the length, diameter, and matrix density. Section 2.02.01.01 further requests impurity analysis on representative samples from the final compact lot, but there are no specified acceptance criteria. The impurity information will be evaluated by INL as part of a final decision on whether to insert the compacts into the AGC-2 experiment. The procedures for characterizing and qualifying the compacts are outlined in ORNL product inspection plan AGR-CHAR-PIP-16. The measurement of compact length, diameter, and matrix density was performed according to data acquisition method AGR-CHAR-DAM-39. The data report forms generated by this procedure document the product acceptance for the property requirements listed in sections 2.03 and 2.04 of SPC-1285. All compacts selected for irradiation conformed to the specified requirements for length, diameter, and density.

In addition to the characterization data, this report also contains other records relevant to the product acceptance. A history of the material flow and sample naming is included and the compacting process is summarized. In addition to results of the impurity analysis on representative samples from the final compact lot, impurity analysis results are also provided for samples of the graphite, resin, and the graphite/resin blend. A Certificate of Conformance to SPC-1285, Rev. 1 is attached in Appendix B.

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### 1 Material identification record for A3-P33

Table 1-1 lists the materials used to make the A3-P33 compacts. The graphite/resin blend was shipped from Babcock and Wilcox (B&W) to ORNL on October 4, 2010. Three completed compacts were shipped to INL on October 28, 2010. Three compacts were also shipped to Shiva Technologies for impurity analysis on October 29, 2010. Fourteen compacts were retained at ORNL. Table 1-2 lists the disposition of each compact. Table 1-3 is a copy of data report form DRF-39B, which lists the specific assignment of final compact ID for each fabricated compact.

Table 1-1: Material identification record for A3-P33 compacts

Sample ID	Parent material	Notes
Blend E	Asbury 3482 natural graphite lot# 7602	Parent material information provided by
	Graftech GTI-D synthetic graphite CAS# 7782-42-5	INL
	Plenco 14433 Batch# 930973	
A3-P33-#	Blend E	Ten cylinders, A3-P33-1 through
		A3-P33-10, pressed from Blend E and
		carbonized
A3-P33-#-A	A3-P33-#	Two compacts machined from each of ten
and		carbonized cylinders, A3-P33-1 through
A3-P33-#-B		A3-P33-10
A3-P33-Z##	A3-P33-#-A	Twenty heat-treated compacts
	and	randomized and relabeled, A3-P33-Z01
	A3-P33-#-B	through A3-P33-Z20 (see DRF-39B for
		specific assignment record)

**Table 1-2: Disposition of A3-P33 compacts** 

Sent to INL	Sent to Shiva		Retained at ORNL	
A3-P33-Z09	A3-P33-Z10	A3-P33-Z01	A3-P33-Z06	A3-P33-Z14
A3-P33-Z20	A3-P33-Z17	A3-P33-Z02	A3-P33-Z07	A3-P33-Z15
A3-P33-Z18 (spare)	A3-P33-Z13	A3-P33-Z03	A3-P33-Z08	A3-P33-Z16
		A3-P33-Z04	A3-P33-Z11	A3-P33-Z19
		A3-P33-Z05	A3-P33-Z12	

Table 1-3. Record of assignment of Z-number to fabricated compacts (DRF-39B)

Data Report Form D	RF-39B: Compact Tracking
Procedure:	AGR-CHAR-DAM-39 Rev. 0
Operator:	John Hunn
Compact lot ID:	A3-P33
Compact Lot description:	Matrix-only compacts from Plenco 14433
Filename:	\\mc-agr\AGR\CompactDimensions\A3-P33_DRF39R0.xls

Compact Z Number	Compact Fat Number	
Z01	3-B	
Z02	5-A	
Z03	3-A	
Z04	2-B	
Z05	2-A	

Compact Z Number	Compact Fab Number
Z06	7-A
Z07	9-B
Z08	10-B
Z09	8-B
Z10	8-A

Compact Z Number	Compact Fab Number
Z11	10-A
Z12	6-B
Z13	7-B
Z14	9-A
Z15	4-A

Compact Z Number	Compact Fab Number
Z16	6-A
Z17	1-A
Z18	5-B
Z19	4-B
Z20	1-B

Comments	

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### 2 <u>Inspection of Length, Diameter, and Matrix Density</u>

At the end of this section is the data report form DRF-39A associated with the compact lot A3-P33. This data report form summarizes the acceptance testing performed according to the product inspection plan AGR-CHAR-PIP-16. The information in this form covers all the property specifications listed in sections 2.03 and 2.04 of SPC-1285. All compacts met the specified criteria for diameter and matrix density. Seven compacts did not meet the specified criteria for length. These compacts were not used. All compacts selected for irradiation or impurity analysis met all dimensional and density specifications. Note that the specification only requires compacts used for irradiation meet these requirements, so the final determination of this inspection is that the product (compacts used for irradiation) conforms to the specified requirements for length, diameter, and density.

Table 2-1 summarizes the critical properties of the compacts selected for possible insertion in the AGC-2 irradiation experiment. Table 2-2 is a copy of data report form DRF-39A.

Table 2-1. Summary of properties of compact shipped for irradiation

Compact ID	Length (mm)	Diameter (mm)	Density (g/cm³)
A3-P33-Z09	6.341	12.72	1.760
A3-P33-Z20	6.315	12.72	1.689
A3-P33-Z18 (spare)	6.339	12.74	1.736
Specification	$6.299 \le x \le 6.350$	$12.700 \le x \le 12.751$	$1.75 \pm 0.13$

Table 2-2. Record of compact acceptance test for dimensions and density (DRF-39A)

# Procedure: AGR-CHAR-DAM-39 Rev. 0 Operator: John Hunn Compact Iot ID: A3-P33 Compact Lot description: Matrix-only compacts from Plenco 14433 Filename: \\mc-agr\AGR\CompactDimensions\A3-P33\_DRF39R0.xls Vertical height gauge calibration due date: 3/22/11 Digital caliper calibration due date: 5/11/11 Gauge blocks calibration due date: 11/7/12 Analytical balance calibration due date: 9/13/11

Acceptance criteria for compact length: ≥6.299 and ≤6.350 mm	
Acceptance criteria for compact diameter: ≥12.700 and ≤12.751 mm	
Acceptance criteria for compact mass: For information only	
Acceptance criteria for compact density: 1.75±0.13 g/cm <sup>3</sup>	

Compact	Mass	Length		Diameter (mm)		Volume	Density	Accept?
ID Number	(g)	(mm)	0°	90°	Average	(cm <sup>3</sup> )	(g/cm³)	(pass or fail
Z01	1.3957	6.347	12.73	12,73	12.73	0.8078	1,7277	pass
Z02	1.4277	6.358	12.73	12.74	12.74	0.8099	1.7629	fail
Z03	1.4291	6.362	12.73	12.73	12.73	0.8097	1.7649	fail
Z04	1,3916	6.352	12.73	12,73	12.73	0.8085	1.7213	fall
Z05	1.4348	6.358	12.74	12.73	12.74	0.8099	1.7717	fail
Z06	1.4338	6.352	12.74	12.73	12.74	0.8091	1.7721	fall
Z07	1.3810	6.310	12.72	12.72	12.72	0.8019	1.7223	pass
Z08	1.4128	6.352	12.73	12.73	12.73	0.8085	1.7475	fall
Z09	1.4182	6.341	12.72	12.72	12.72	0.8058	1.7600	pass
Z10	1.4355	6.346	12.74	12.74	12.74	0.8090	1.7745	pass
Z11	1.4345	6.343	12.73	12.73	12.73	0.8073	1.7769	pass
Z12	1.3827	6.324	12.71	12.71	12.71	0.8024	1.7233	pass
Z13	1.3984	6.341	12.72	12.72	12.72	0.8058	1.7354	pass
Z14	1,4323	6.353	12.73	12.73	12.73	0.8086	1.7714	Fail
Z15	1.4314	6.337	12.74	12.73	12.74	0.8072	1.7733	pass
Z16	1,4145	6.343	12.72	12.72	12.72	0.8060	1.7549	pass
Z17	1.4053	6.338	12.74	12.74	12.74	0.8079	1.7394	pass
Z18	1.4019	6.339	12.73	12.74	12.74	0.8074	1.7362	pass
Z19	1.4077	6.343	12.73	12.73	12.73	0.8073	1.7437	pass
Z20	1.3550	6.315	12.72	12.72	12.72	0.8025	1.6885	pass

Comments	
Seven compacts failed length specification (too long). These will not be used. All but two compacts had side fissures and end damage. 209 and 220 have the best surface appearance and will be shipped for irradiation. 209 did have minor end damage. 218 had minor side fissures, it will be shipped as a spare.	

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### 3 Inspection of Compact Surface Appearance

All but 2 compacts had obvious surface fissures on the sides (Figure 3-1) and surface damage on one or both ends (Figure 3-2). The compact shown in Figure 3-3 through Figure 3-5 had a side fissure that was connected to a crack across the top of the compact. Two of the compacts that did not have obvious surface fissures were selected for irradiation (see Table 1-2). However, one of these compacts still showed some damage on one end face (Figure 3-6). A third compact was selected as a spare, based on the fact that it only exhibited minor side fissures.

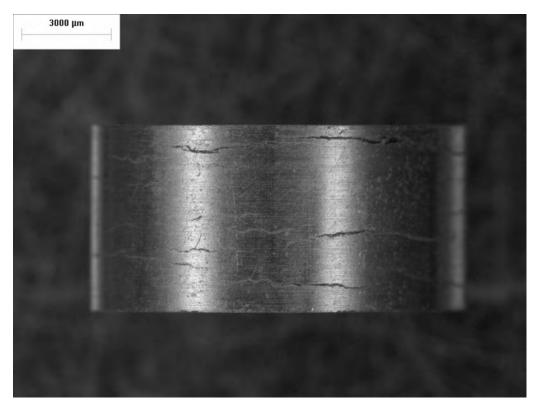


Figure 3-1. Fissures were observed to a varying degree on the sides of most compacts. An example of side fissures on compact A3-H08-Z04 from a similar compact lot is shown.

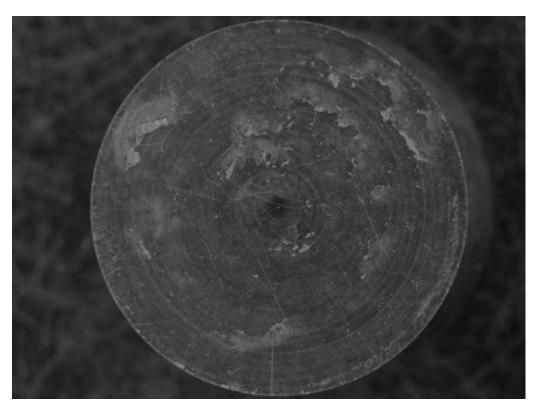


Figure 3-2. End faces of many compacts showed damage that looked like flakes of material were delaminating and sometimes breaking away. Compact A3-H08-Z04 is shown.

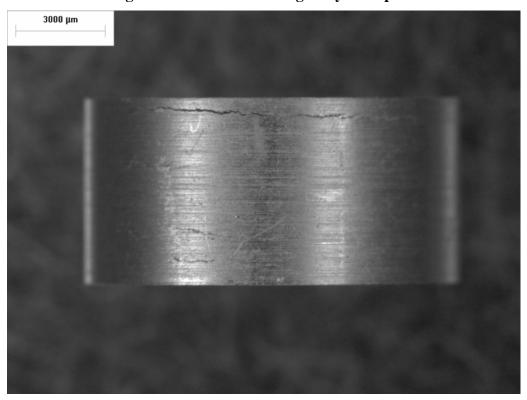


Figure 3-3. Side fissure on compact A3-P33-Z08.

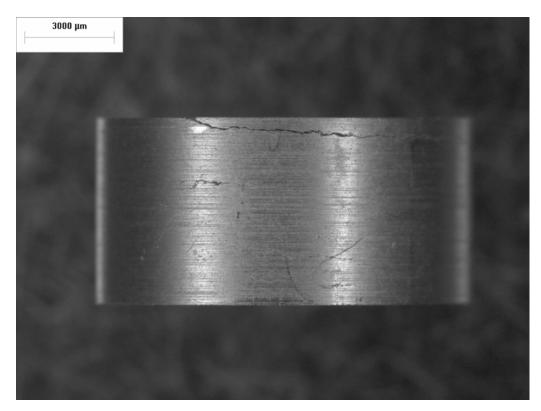


Figure 3-4. Another rotation of compact A3-P33-Z08 showing side fissure.

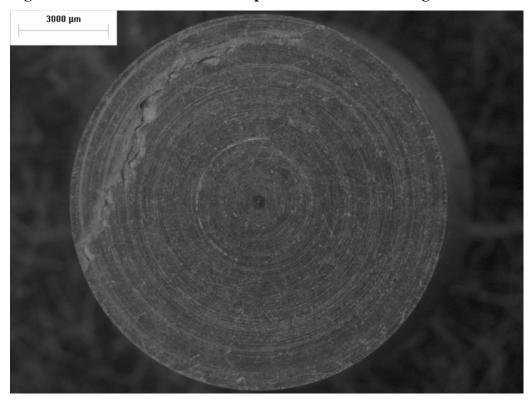


Figure 3-5. Compact A3-P33-Z08 is shown, where the fissure observed on the side can be seen to continue as a crack across the top of the compact.

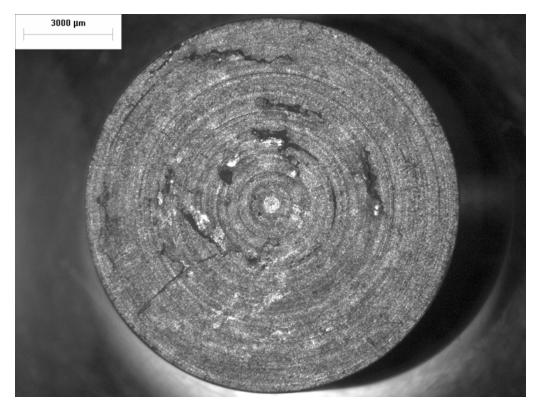


Figure 3-6. One end of A3-P33-Z09 (selected for irradiation) showed some surface damage on one end.

### 4 Compacting process conditions

Initial matrix-only compacting tests were performed using parameters suggested by INL, which were selected based on manufacturer provided resin properties and previous experiments with overcoated material. These test compacts exhibited problems including delamination or fracture during ejection from the die and development of fissures during carbonization. The higher fraction of resin in the matrix-only compacts compared to compacts made from overcoated particles may have been a contributing factor to the difficulties encountered. To reduce the observed cracking, additional development was carried out before the final matrix-only compacts were fabricated. As part of this development, several compacts were made at various pressing conditions to determine the most effective fabrication methods. A summary of the final fabrication procedure is outlined below. This procedure was able to produce compacted cylinders with minimal visible flaws in the as-compacted (green) state. However, fissures still developed during carbonization.

AGC-2 matrix-only compacts needed to be nominally 12.7 mm in diameter, 6.35 mm in length, and 1.75 g/cm<sup>3</sup> in density. Normally, a custom die would be made to produce compacts with the required dimensions. However, a limited time was available for fabrication of these compacts in order to have them available for inclusion in the AGC-2 irradiation test. The required fabrication schedule made it infeasible to obtain a new compacting die with a diameter that would yield the desired final compact diameter after heat-treatment. As an alternative approach, a slightly oversized (15.24 mm diameter) die was used to produce 10 cylinders from each matrix blend that were then machined into the final 20 compacts. The die was single-acting, that is, the top punch moved and the bottom punch was fixed. To obtain two compacts from each carbonized cylinder, a minimum length of at least 25.4 mm long was desired to allow for gripping of the cylinder and machining loss. However, the compacting die, which had ~75 mm of available length for loading, was not tall enough to hold the amount of as-received matrix precursor powder required to produce a compacted cylinder at least 25.4 mm long. The jet milled powder had a low bulk density, so a pre-compacting method for the as-received powder was developed to allow the required amount of feed material to fit in the available die. Another die (25.4 mm diameter) was used to produce ~1 g/cm<sup>3</sup> slugs, which were re-granulated into a coarse powder that would work with the 15.24 mm diameter compacting die. These low density slugs were made by filling the 25.4 mm diameter die at room temperature with the as-received matrix precursor blend and pressing to 8 kN. The slugs were then broken into granules and passed through a U.S. Standard #20 (850  $\mu$ m nominal opening) sieve to remove any large chunks.

Table 4-1 provides a summary of the critical steps in the compacting schedule. All AGC-2 matrix-only compacts were made using standard operating procedure AGR-COMP-SOP-10, "Production of AGC Irradiation Specimens" and the following pressing schedule. Using the precompacting method described above, charges were prepared and weighed out while the compacting die, top punch, and bottom punch were heated simultaneously to 130±1°C. The compact charge weight was calculated to produce a compact of the required length and density, based on empirical data on weight loss and shrinkage. During heating, the inner diameter and contact surfaces of the top and bottom punches were lightly sprayed with McLube 860 mold release agent and allowed to dry. The charge was poured into the compacting die within an approximately 30 second long period. The top punch was put in place and the matrix precursor

material was allowed to warm up in the die for an additional 20-30 seconds before the programmed compacting sequence was initiated on the Promess press. The press ram was advanced at 1 mm/sec, taking approximately 20 seconds to reach the target position. This target position was chosen to produce a compact of the desired length. At 1 mm short of the target position, there was a 1 second delay. This delay provided additional relaxation time for the material and reduced the peak force applied during compacting. After the 1 second delay, the press continued to move to the target position. Once at the target position, the press held position for 60 seconds. After the hold, the press retracted and an ejection block was set in place to allow the lower punch and cylinder to be ejected from the bottom of the die.

**Table 4-1. Compacting schedule summary** 

Step	Action Timing		Comments
1	Load die	~30 sec to load	
2	Delay	~30 sec	Allow matrix precursor material to heat up
3	Initiate program		
4	Move to position	~20 sec	Pressing at 1 mm/sec
5	Delay	1 sec	Hold position 1 mm short of target position
6	Move to position	1 sec	Continue to target position at 1mm/sec
7	Delay	60 sec	Hold position
8	Move to position	N/A	Retract for ejection
9	Move to position	N/A	Eject part at 3 mm/sec

The compacted cylinders were carbonized per procedure AGR-COMP-SOP-04, "Carbonizing Compacts" by heating to 950°C at a rate of 1°C/min in flowing helium, followed by a 1 hour hold. The carbonized cylinders were machined according to drawing AGR-COMP-DWG-03, "AGC Compact Drawing" (see appendix A). Cylinders were first turned down to the target diameter. Prior to cutting two compacts of the target length from each cylinder, a thin layer of material was removed from the end to square the cylinder. The two machined compacts were identified by adding "A" or "B" to the fabrication ID relative to their location within the original compact (A being closest to the top of the die). Most of the B compacts came from near the middle of the cylinder. However, one of the compacted cylinders fractured during carbonization (see Table 4-2). For this cylinder, the B compact was taken from closer to the bottom of the cylinder. After machining, the compacts were heat-treated per procedure AGR-COMP-SOP-05, "Heat-treating Compacts" by heating to 1800°C under vacuum at a rate of 20°C/min, followed by a 1 hour hold. The main purpose of the heat-treatment process was to reduce impurity content in the compacts. Compacts were heat-treated after machining to reduce the potential for contamination after the heat-treatment step.

Based on previous experience with AGR matrix materials, most dimensional changes in the pressed cylinders were expected to occur during carbonization. However, compacts can also undergo dimensional changes during heat-treatment. These changes are usually a consistent minor shrinkage and can be compensated for by using empirical data to oversize the compacts. During initial testing, it was determined that the dimensional change induced by the heat-treatment of the A3-P33 matrix material was inconsistent. Some test compacts shrank, while others grew in length. For this reason, compacts were machined to a length close to the middle of the specified final length for the heat-treated compacts. This provided the most flexibility and

allowed for re-machining of compacts that were too long. Upon inspection of the heat-treated compacts, there were enough compacts with an acceptable length, so re-machining was not necessary.

Table 4-2 provides dimensional analysis for the cylinders before and after carbonization. Table 4-3 provides dimensional analysis for the machined compacts before and after heat-treatment. Table 4-2 also lists the compaction force required to press each green compact. Average density was determined from the measured weight and dimensions assuming a cylindrical geometry. One cylinder could not be measured after carbonization because it fractured during the carbonization process.

Because of the presence of fissures in the cylinders and compacts, it is difficult to draw conclusions from the analysis of the data in Table 4-2 and Table 4-3. These fissures were visible in most of the final heat-treated compacts and are discussed in section 3. These fissures can add to the length of the compact and produce an error in the calculated density.

Fractional weight loss after carbonization was consistent in all the cylinders that were measured. Fractional change in length after carbonization was less consistent due to the presence of fissures in the cylinders. Table 4-3 shows that many of the machined compacts were longer after heat-treatment. This was also most likely due to the formation or expansion of these fissures. There was also a slight weight loss after heat-treatment. The calculated density of the compacts taken from closer to the top of the cylinder was higher than those taken from lower down because the compacting force was greater closer to the moving punch.

Table 4-2. Analysis of cylinders before and after carbonization

		Green				Carbonized				Fractional cl	nange from g	reen to carb	onized
Fabrication ID	Compaction Force (Mpa)	Length (mm)	Dia (mm)	Mass (g)	Density (g/cm²)	Length (mm)	Dia (mm)	Mass (g)	Density (g/cm²)	Length	Dia	Mass	Density
A3-P33-1	33.3	26.12	15.23	8.4096	1.767	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
A3-P33-2	31.0	25.93	15.24	8.4180	1.780	25.22	15.02	7.7499	1.734	0.973	0.986	0.921	0.974
A3-P33-3	32.8	25.95	15.24	8.4050	1.776	25.18	15.04	7.7385	1.730	0.970	0.987	0.921	0.974
A3-P33-4	35.3	25.73	15.24	8.4087	1.792	25.14	14.99	7.7465	1.746	0.977	0.984	0.921	0.975
A3-P33-5	33.5	25.90	15.22	8.4168	1.786	25.15	15.03	7.7503	1.737	0.971	0.988	0.921	0.972
A3-P33-6	31.2	25.89	15.20	8.4131	1.791	25.36	15.06	7.7588	1.718	0.980	0.991	0.922	0.959
A3-P33-7	33.1	25.80	15.20	8.4099	1.796	25.11	15.03	7.7504	1.740	0.973	0.989	0.922	0.968
A3-P33-8	36.7	25.68	15.22	8.4064	1.799	25.09	15.04	7.7435	1.737	0.977	0.988	0.921	0.966
A3-P33-9	30.1	25.85	15.25	8.4143	1.782	25.20	15.05	7.7524	1.729	0.975	0.987	0.921	0.970
A3-P33-10	33.4	25.69	15.20	8.4102	1.804	25.10	15.00	7.7458	1.746	0.977	0.987	0.921	0.968

N/A = Not applicable (carbonized length could not be determined because cylinder broke during carbonization)

Table 4-3: Analysis of machined compacts before and after heat-treatment

	Carbonized				Heat Treated				Fractional change from carbonized to heat treated				
Fabrication ID	Characterization ID	Length (mm)	Dia (mm)	Mass (g)	Density (g/cm²)	Length (mm)	Dia (mm)	Mass (g)	Density (g/cm²)	Length	Dia	Mass	Density
A3-P33-1-A	A3-P33-Z17	6.32	12.72	1.4115	1.7575	6.338	12.74	1.4053	1.7394	1.003	1.002	0.996	0.990
A3-P33-1-B	A3-P33-Z17	6.33	12.72	1.3626	1.6939	6.315	12.72	1.3550	1.6885	0.998	1.002	0.994	0.997
A3-P33-2-A	A3-P33-Z05	6.33	12.72	1.4405	1.7908	6.358	12.74	1.4348	1.7703	1.004	1.002	0.996	0.989
A3-P33-2-B	A3-P33-Z04	6.34	12.72	1.3985	1.7358	6.352	12.73	1.3916	1.7213	1.002	1.001	0.995	0.992
A3-P33-3-A	A3-P33-Z03	6.33	12.72	1.4351	1.7841	6.362	12.73	1.4291	1.7649	1.005	1.001	0.996	0.989
A3-P33-3-B	A3-P33-Z01	6.34	12.72	1.4025	1.7408	6.347	12.73	1.3957	1.7277	1.001	1.001	0.995	0.992
A3-P33-4-A	A3-P33-Z15	6.31	12.72	1.4373	1.7925	6.337	12.74	1.4314	1.7719	1.004	1.002	0.996	0.989
A3-P33-4-B	A3-P33-Z19	6.33	12.72	1.4146	1.7586	6.343	12.73	1.4077	1.7437	1.002	1.001	0.995	0.992
A3-P33-5-A	A3-P33-Z02	6.34	12.72	1.4334	1.7792	6.358	12.73	1.4277	1.7643	1.003	1.001	0.996	0.992
A3-P33-5-B	A3-P33-Z18	6.33	12.72	1.4086	1.7511	6.339	12.73	1.4019	1.7376	1.001	1.001	0.995	0.992
A3-P33-6-A	A3-P33-Z16	6.33	12.72	1.4231	1.7692	6.343	12.72	1.4145	1.7549	1.002	1.000	0.994	0.992
A3-P33-6-B	A3-P33-Z12	6.33	12.72	1.3914	1.7298	6.324	12.71	1.3827	1.7233	0.999	0.999	0.994	0.996
A3-P33-7-A	A3-P33-Z06	6.33	12.72	1.4414	1.7919	6.352	12.74	1.4338	1.7707	1.003	1.002	0.995	0.988
A3-P33-7-B	A3-P33-Z13	6.33	12.72	1.4062	1.7482	6.341	12.72	1.3984	1.7354	1.002	1.000	0.994	0.993
A3-P33-8-A	A3-P33-Z10	6.32	12.73	1.4421	1.7928	6.346	12.74	1.4355	1.7745	1.004	1.001	0.995	0.990
A3-P33-8-B	A3-P33-Z09	6.33	12.72	1.4256	1.7723	6.341	12.72	1.4182	1.7600	1.002	1.000	0.995	0.993
A3-P33-9-A	A3-P33-Z14	6.33	12.72	1.4383	1.7881	6.353	12.73	1.4323	1.7714	1.004	1.001	0.996	0.991
A3-P33-9-B	A3-P33-Z07	6.31	12.72	1.3866	1.7292	6.310	12.72	1.3810	1.7223	1.000	1.000	0.996	0.996
A3-P33-10-A	A3-P33-Z11	6.33	12.72	1.4401	1.7903	6.343	12.73	1.4345	1.7769	1.002	1.001	0.996	0.993
A3-P33-10-B	A3-P33-Z08	6.33	12.72	1.4196	1.7648	6.352	12.73	1.4128	1.7475	1.003	1.001	0.995	0.990

### 5 Impurity analysis of matrix, resin, and graphite

Samples of the natural and synthetic graphite, resin, and matrix precursor blend E were sent to Shiva Technologies for impurity analysis. The matrix precursor powder for compact lot A3-P33 was a jet milled blend of 64 wt% natural graphite (Asbury 3482), 16 wt% synthetic graphite (Graftech GTI-D), and 20 wt% of a developmental novolac resin (Plenco 14433). The resin and matrix precursor blend were carbonized prior to shipment to Shiva. The carbonization process was used to remove volatiles that would interfere with the impurity analysis. Approximately 5 grams of resin and graphite/resin blend were loaded into separate quartz trays and then placed into a tube furnace. The samples were heated to 950°C at a rate of 5°C/min and held at 950°C for 1 hour. The furnace power was cut and the samples cooled to room temperature. The samples were then loaded into glass vials and shipped to SHIVA for full scan glow discharge mass spectrometry (GDMS) analysis, along with samples of the natural and synthetic graphite.

Table 5-1 is a compilation of the impurity analysis results. Impurities that could not be detected above the analysis threshold value are reported as less than values (<) and appear in gray. Values marked as less than or equal to (=<) indicate that a measurable value of the element was obtained, but that this element may have come from the Shiva sample preparation. Prior to GDMS analysis, Shiva poured the powder samples into a Teflon mold with a binder material. The binder was mostly indium, but may also have contained other elements, as indicated in the analysis report by the "=<" symbol. The resin and graphite/resin blend showed high values for F, but these were marked as semiquantitative (~) and probably came from the Teflon mold. The natural graphite was very high in Si and also high in Mg, Al, S, and Fe. The synthetic graphite was high in Cu. The impurities in the graphite carried over to the jet milled blend. The resin had high levels of Mg, Al, Si, S, and Ca that appeared to also carry over into the jet milled blend. There was also a higher fraction of Fe and Ni in the graphite/resin blend than would be expected based on the analysis of the graphite and resin alone. This additional Fe and Ni were not seen in the other matrix precursor blends used to make matrix-only compacts for the AGC-2 irradiation experiment.

Copies of the Shiva Technologies certified impurity analysis data sheets for the natural and synthetic graphite are provided in Table 5-2 and Table 5-3. A copy of the certified impurity analysis data sheet for the Plenco resin is provided in Table 5-4. A copy of the certified impurity analysis data sheet for the graphite/resin blend made from these materials (INL Blend E) is provided in Table 5-5.

Samples of the final heat treated compacts were also sent to Shiva for analysis. These results are presented in section 6. As discussed in that section, heat-treatment of the compacts removed some of the impurities present in the graphite/resin blend.

**Table 5-1. Summary of feedstock impurities** 

T21 4	Concentration (ppm wt)							
Element	Asbury 3482	GTI-D	Plenco 14433	INL Blend E				
Li	< 0.01	< 0.01	3.6	0.39				
Be	< 0.01	< 0.01	< 0.01	< 0.01				
В	0.24	0.77	0.24	0.6				
C	Matrix	Matrix	Matrix	Matrix				
N	-	-	-	-				
О	-	-	-	-				
F	~ 20	~ 10	~ 180	~ 180				
Na	1.5	11	62	7				
Mg	80	1.2	45	78				
Al	29	0.9	100	44				
Si	710	2.7	250	710				
P	0.82	< 0.1	1.3	1.7				
S	25	10	340	50				
C1	2.5	7.8	3.5	8.5				
K	0.2	< 0.1	1.1	1				
Ca	8.2	3.2	770	140				
Sc	< 0.05	< 0.05	< 0.05	< 0.05				
Ti	2.3	2.2	3.6	2.5				
V	0.45	9.9	0.05	2.4				
Cr	< 0.5	< 0.5	< 0.5	14				
Mn	0.55	< 0.05	0.19	1.2				
Fe	38	1.1	8.2	80				
Co	< 0.05	< 0.05	< 0.05	0.29				
Ni	0.25	0.25	0.14	20				
Cu	2.5	120	7.5	47				
Zn	0.4	< 0.1	=< 1.2	< 0.1				
Ga	< 0.1	< 0.1	< 0.1	< 0.1				
Ge	< 0.1	< 0.1	< 0.1	< 0.1				
As	< 0.1	< 0.1	< 0.1	< 0.1				
Se	< 0.1	< 0.1	< 0.1	< 0.1				
Br	0.41	< 0.1	< 0.1	1.5				
Rb	< 0.05	< 0.05	=< 0.1	< 0.05				
Sr	0.08	< 0.05	0.46	0.15				
Y	0.2	< 0.05	< 0.05	0.45				
Zr	0.6	0.14	< 0.05	2.6				
Nb	< 0.1	< 0.1	< 0.1	< 0.1				
Mo	< 0.05	0.09	0.06	0.8				
Ru	< 0.1	< 0.1	< 0.1	< 0.1				
Rh	< 0.1	< 0.1	< 0.1	< 0.1				
Pd	< 0.1	< 0.1	< 0.1	< 0.1				
Ag	< 0.1	< 0.1	< 0.1	< 0.1				
Cd	< 0.1	< 0.1	< 0.1	< 0.1				
In	Binder	Binder	Binder	Binder				

**Table 5-1. Summary of feedstock impurities (continued)** 

T21 /	Concentration (ppm wt)								
Element	Asbury 3482	GTI-D	Plenco 14433	INL Blend E					
Sn	< 0.5	< 0.5	< 0.5	< 0.5					
Sb	< 0.5	< 0.5	< 0.5	< 0.5					
Те	< 0.1	< 0.1	< 0.1	< 0.1					
I	< 20	=< 80	< 20	=< 30					
Cs	< 0.1	< 0.1	< 0.1	< 0.1					
Ba	0.8	< 0.1	< 0.1	1.8					
La	< 0.5	=< 2	=< 3.5	< 0.5					
Се	< 0.5	< 0.5	< 0.5	< 0.5					
Pr	< 0.05	< 0.05	=< 0.55	< 0.05					
Nd	< 0.05	< 0.05	< 0.05	< 0.05					
Sm	< 0.05	< 0.05	< 0.05	< 0.05					
Eu	< 0.05	< 0.05	< 0.05	< 0.05					
Gd	< 0.05	< 0.05	< 0.05	< 0.05					
Tb	< 0.05	< 0.05	< 0.05	< 0.05					
Dy	< 0.05	< 0.05	< 0.05	< 0.05					
Но	< 0.05	< 0.05	< 0.05	< 0.05					
Er	< 0.05	< 0.05	< 0.05	< 0.05					
Tm	< 0.05	< 0.05	< 0.05	< 0.05					
Yb	< 0.05	< 0.05	< 0.05	< 0.05					
Lu	< 0.05	< 0.05	< 0.05	< 0.05					
Hf	< 0.05	< 0.05	< 0.05	< 0.05					
Ta	< 5	< 5	< 5	< 5					
W	0.15	< 0.05	< 0.05	0.7					
Re	< 0.05	< 0.05	< 0.05	< 0.05					
Os	< 0.05	< 0.05	< 0.05	< 0.05					
Ir	< 0.05	< 0.05	< 0.05	< 0.05					
Pt	< 0.05	< 0.05	< 0.05	< 0.05					
Au	< 0.1	< 0.1	< 0.1	< 0.1					
Hg	< 0.5	< 0.5	< 0.5	< 0.5					
T1	< 0.1	< 0.1	< 0.1	< 0.1					
Pb	< 0.5	< 0.5	< 0.5	< 0.5					
Bi	< 0.1	< 0.1	< 0.1	< 0.1					
Th	< 0.05	< 0.05	< 0.05	< 0.05					
U	< 0.05	< 0.05	< 0.05	< 0.05					

Table 5-2. Impurity analysis report for Asbury 3482 natural graphite lot# 7602



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SHIVA Technologies An Operating Unit of Evans Analytical Group LLC 6707 Brooklawn Parkway Syracuse, New York 13211 Telephone (315) 431-9900 Fax: (315) 431-9800 Email info.ny@eaglabs.com www.eaglabs.com

Customer: UT-Battelle Oak Ridge

P.O.#

4000100480

1 Bethel Valley Rd, Oak Ridge, TN 37823-6063 USA Date: 6-Nov-10

Job #

S0ABV776

Customer ID: C

Sample ID:

S101101057

Asbury 3482 NFG

Element	Concentration [ ppm wt ]	Element	Concentration [ ppm wt ]
Li	< 0.01	Pd	< 0.1
Ве	< 0.01	Ag	< 0.1
В	0.24	Cd	< 0.1
С	Matrix	In	Binder
N	-	Sn	< 0.5
0	-	Sb	< 0.5
F	~ 20	Те	< 0.1
Na	1.5		< 20
Mg	80	Cs	< 0.1
Al	29	Ва	0.8
Si	710	La	< 0.5
Р	0.82	Ce	< 0.5
S	25	Pr	< 0.05
CI	2.5	Nd	< 0.05
K	0.2	Sm	< 0.05
Ca	8.2	Eu	< 0.05
Sc	< 0.05	Gd	< 0.05
Ti	2.3	Tb	< 0.05
V	0.45	Dy	< 0.05
Cr	< 0.5	Но	< 0.05
Mn	0.55	Er	< 0.05
Fe	38	Tm	< 0.05
Co	< 0.05	Yb	< 0.05
Ni	0.25	Lu	< 0.05
Cu	2.5	Hf	< 0.05
Zn	0.4	Та	< 5
Ga	< 0.1	W	0.15
Ge	< 0.1	Re	< 0.05
As	< 0.1	Os	< 0.05
Se	< 0.1	lr	< 0.05
Br	0.41	Pt	< 0.05
Rb	< 0.05	Au	< 0.1
Sr	0.08	Hg	< 0.5
Y	0.2	TĪ	< 0.1
Zr	0.6	Pb	< 0.5
Nb	< 0.1	Bi	< 0.1
Мо	< 0.05	Th	< 0.05
Ru	< 0.1	U	< 0.05
Rh	< 0.1		

<sup>~</sup> Semiquantitative Values

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Table 5-3. Impurity analysis report for Graftech GTI\_D synthetic graphite #7782-42-5



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Customer: UT-Battelle Oak Ridge

P.O.# 4000100480

1 Bethel Valley Rd, Oak Ridge, TN 37823-6063 USA 6-Nov-10

Job # S0ABV776

Customer ID: C

Sample ID: \$101101058

**GTI-D-SG** 

Element	Concentration [ ppm wt ]	Element	Concentration [ ppm wt ]
Li	< 0.01	Pd	< 0.1
Be	< 0.01	Ag	< 0.1
В	0.77	Cd	< 0.1
С	Matrix	ln	Binder
N	=	Sn	< 0.5
0	=	Sb	< 0.5
F	~ 10	Te	< 0.1
Na	11	I	=< 80
Mg	1.2	Cs	< 0.1
Al	0.9	Ва	< 0.1
Si	2.7	La	=< 2
Р	< 0.1	Ce	< 0.5
S	10	Pr	< 0.05
Cl	7.8	Nd	< 0.05
K	< 0.1	Sm	< 0.05
Ca	3.2	Eu	< 0.05
Sc	< 0.05	Gd	< 0.05
Ti	2.2	Tb	< 0.05
V	9.9	Dy	< 0.05
Cr	< 0.5	Но	< 0.05
Mn	< 0.05	Er	< 0.05
Fe	1.1	Tm	< 0.05
Co	< 0.05	Yb	< 0.05
Ni	0.25	Lu	< 0.05
Cu	120	Hf	< 0.05
Zn	< 0.1	Та	< 5
Ga	< 0.1	W	< 0.05
Ge	< 0.1	Re	< 0.05
As	< 0.1	Os	< 0.05
Se	< 0.1	lr	< 0.05
Br	< 0.1	Pt	< 0.05
Rb	< 0.05	Au	< 0.1
Sr	< 0.05	Hg	< 0.5
Y	< 0.05	TI	< 0.1
Zr	0.14	Pb	< 0.5
Nb	< 0.1	Bi	< 0.1
Mo	0.09	Th	< 0.05
Ru	< 0.1	U	< 0.05
Rh	< 0.1		

<sup>~</sup> Semiquantitative Values

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Table 5-4. Impurity analysis report for Plenco 14433 batch# 930973



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Customer: **UT-Battelle Oak Ridge**  P.O.#

4000100480

1 Bethel Valley Rd, Oak Ridge, TN 37823-6063 USA 6-Nov-10

Job#

S0ABV776

Customer ID: C

Sample ID:

S101101060

**Plenco 14433** 

Element	Concentration [ ppm wt ]	Element	Concentration [ ppm wt ]
Li	3.6	Pd	< 0.1
Be	< 0.01	Ag	< 0.1
В	0.24	Cd	< 0.1
С	Matrix	ln	Binder
N	-	Sn	< 0.5
0	-	Sb	< 0.5
F	~ 180	Te	< 0.1
Na	62	I	< 20
Mg	45	Cs	< 0.1
Al	100	Ва	< 0.1
Si	250	La	=< 3.5
Р	1.3	Ce	< 0.5
S	340	Pr	=< 0.55
CI	3.5	Nd	< 0.05
K	1.1	Sm	< 0.05
Ca	770	Eu	< 0.05
Sc	< 0.05	Gd	< 0.05
Ti	3.6	Tb	< 0.05
V	0.05	Dy	< 0.05
Cr	< 0.5	Но	< 0.05
Mn	0.19	Er	< 0.05
Fe	8.2	Tm	< 0.05
Co	< 0.05	Yb	< 0.05
Ni	0.14	Lu	< 0.05
Cu	7.5	Hf	< 0.05
Zn	=< 1.2	Та	< 5
Ga	< 0.1	W	< 0.05
Ge	< 0.1	Re	< 0.05
As	< 0.1	Os	< 0.05
Se	< 0.1	lr	< 0.05
Br	< 0.1	Pt	< 0.05
Rb	=< 0.1	Au	< 0.1
Sr	0.46	Hg	< 0.5
Υ	< 0.05	TI	< 0.1
Zr	< 0.05	Pb	< 0.5
Nb	< 0.1	Bi	< 0.1
Mo	0.06	Th	< 0.05
Ru	< 0.1	U	< 0.05
Rh	< 0.1		

<sup>~</sup> Semiquantitative Values

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Table 5-5. Impurity analysis report for INL graphite/resin Blend E



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Customer: UT-Battelle Oak Ridge

P.O.#

4000100480

1 Bethel Valley Rd, Oak Ridge, TN 37823-6063 USA 7-Nov-10

Job #

S0ABV776

Customer ID: C

Sample ID:

S101101064

**INL Blend E** 

Element	Concentration [ ppm wt ]	Element	Concentration [ ppm wt ]
Li	0.39	Pd	< 0.1
Be	< 0.01	Ag	< 0.1
В	0.6	Cd	< 0.1
С	Matrix	In	Binder
N	-	Sn	< 0.5
0	-	Sb	< 0.5
F	~ 180	Te	< 0.1
Na	7		=< 30
Mg	78	Cs	< 0.1
ΑĬ	44	Ва	1.8
Si	710	La	< 0.5
Р	1.7	Ce	< 0.5
S	50	Pr	< 0.05
CI	8.5	Nd	< 0.05
K	1	Sm	< 0.05
Ca	140	Eu	< 0.05
Sc	< 0.05	Gd	< 0.05
Ti	2.5	Tb	< 0.05
V	2.4	Dy	< 0.05
Cr	14	Ho	< 0.05
Mn	1.2	Er	< 0.05
Fe	80	Tm	< 0.05
Co	0.29	Yb	< 0.05
Ni	20	Lu	< 0.05
Cu	47	Hf	< 0.05
Zn	< 0.1	Та	< 5
Ga	< 0.1	W	0.7
Ge	< 0.1	Re	< 0.05
As	< 0.1	Os	< 0.05
Se	< 0.1	lr	< 0.05
Br	1.5	Pt	< 0.05
Rb	< 0.05	Au	< 0.1
Sr	0.15	Hg	< 0.5
Y	0.45	ΤΪ	< 0.1
Zr	2.6	Pb	< 0.5
Nb	< 0.1	Bi	< 0.1
Мо	0.8	Th	< 0.05
Ru	< 0.1	U	< 0.05
Rh	< 0.1		

<sup>~</sup> Semiquantitative Values

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### **6** Inspection of heat-treated compact impurities

Three heat-treated compacts were sent to Shiva Technologies for impurity analysis (see Table 1-2). Although not required by the specification, these compacts also met the requirements for diameter, length, and density placed on the compacts used for irradiation. Where possible within this limitation, compacts were selected that were machined from the same pressed cylinders as the compacts selected for irradiation.

Table 6-1 is a compilation of the impurity analysis results. The impurities in the feedstock materials were discussed in section 5. For comparison, Table 6-1 includes the impurity analysis for the matrix blend E used to make the A3-P33 compacts. Impurities that could not be detected above the analysis threshold value are reported as less than values (<) and appear in gray. There is no indication that the compacting process significantly increased any of the impurity levels in the heat-treated matrix-only compacts above what was already in the matrix precursor. Some impurities were significantly reduced by the heat-treatment (e.g., Na, Cl, Cr, Fe, Ni, and Cu). Mg was reduced, but not as significantly. Other impurities present at moderate levels in the graphite/resin blend seemed to be somewhat reduced but were still preset at moderate levels (e.g., Al, S, and Ca). The very high Si content from the natural graphite was reduced by about 24-54% in the heat-treated compacts, but was still very high.

Copies of the Shiva Technologies certified impurity analysis data sheets for the three heat-treated compacts are provided in Table 6-2, Table 6-3, and Table 6-4.

**Table 6-1. Summary of heat-treated compact impurities** 

	Concentration (ppm wt)							
Element	A3-P33-Z10	A3-P33-Z13	A3-P33-Z17	INL Blend E				
Li	< 0.01	< 0.01	< 0.01	0.39				
Be	< 0.01	< 0.01	< 0.01	< 0.01				
В	0.12	0.06	0.12	0.6				
С	Matrix	Matrix	Matrix	Matrix				
N	-	-	-	-				
0	-	-	-	-				
F	< 1	< 1	< 1	~ 180				
Na	< 0.05	< 0.05	< 0.05	7				
Mg	6.2	3.2	12	78				
Al	22	14	31	44				
Si	410	330	540	710				
P	1	0.66	1.3	1.7				
S	26	25	47	50				
C1	0.18	0.07	0.44	8.5				
K	< 0.1	< 0.1	< 0.1	1				
Ca	16	17	110	140				
Sc	< 0.05	< 0.05	< 0.05	< 0.05				
Ti	0.51	0.31	2.7	2.5				
V	0.36	0.22	1.7	2.4				
Cr	< 0.5	< 0.5	< 0.5	14				
Mn	< 0.05	< 0.05	< 0.05	1.2				
Fe	0.05	0.08	0.09	80				
Co	< 0.05	< 0.05	< 0.05	0.29				
Ni	< 0.1	< 0.1	< 0.1	20				
Cu	< 0.1	< 0.1	< 0.1	47				
Zn	< 0.1	< 0.1	< 0.1	< 0.1				
Ga	< 0.1	< 0.1	< 0.1	< 0.1				
Ge	< 0.1	< 0.1	< 0.1	< 0.1				
As	< 0.1	< 0.1	< 0.1	< 0.1				
Se	< 0.1	< 0.1	< 0.1	< 0.1				
Br	< 0.1	< 0.1	< 0.1	1.5				
Rb	< 0.05	< 0.05	< 0.05	< 0.05				
Sr	< 0.05	< 0.05	0.08	0.15				
Y	< 0.05	< 0.05	0.13	0.45				
Zr	0.5	0.22	1.9	2.6				
Nb	< 0.1	< 0.1	< 0.1	< 0.1				
Mo	0.11	0.1	0.25	0.8				
Ru	< 0.1	< 0.1	< 0.1	< 0.1				
Rh	< 0.1	< 0.1	< 0.1	< 0.1				
Pd	< 0.1	< 0.1	< 0.1	< 0.1				
Ag	< 0.1	< 0.1	< 0.1	< 0.1				
Cd	< 0.1	< 0.1	< 0.1	< 0.1				
In	< 0.1	< 0.1	< 0.1	Binder				

**Table 6-1. Summary of heat-treated compact impurities (continued)** 

TIL 4	Concentration (ppm wt)							
Element	A3-P33-Z10	A3-P33-Z13	A3-P33-Z17	INL Blend E				
Sn	< 0.5	< 0.5	< 0.5	< 0.5				
Sb	< 0.5	< 0.5	< 0.5	< 0.5				
Те	< 0.1	< 0.1	< 0.1	< 0.1				
I	< 0.1	< 0.1	< 0.1	=< 30				
Cs	< 0.1	< 0.1	< 0.1	< 0.1				
Ba	< 0.1	< 0.1	0.34	1.8				
La	< 0.5	< 0.5	< 0.5	< 0.5				
Се	< 0.05	< 0.05	< 0.05	< 0.5				
Pr	< 0.05	< 0.05	< 0.05	< 0.05				
Nd	< 0.05	< 0.05	< 0.05	< 0.05				
Sm	< 0.05	< 0.05	< 0.05	< 0.05				
Eu	< 0.05	< 0.05	< 0.05	< 0.05				
Gd	< 0.05	< 0.05	< 0.05	< 0.05				
Tb	< 0.05	< 0.05	< 0.05	< 0.05				
Dy	< 0.05	< 0.05	< 0.05	< 0.05				
Но	< 0.05	< 0.05	< 0.05	< 0.05				
Er	< 0.05	< 0.05	< 0.05	< 0.05				
Tm	< 0.05	< 0.05	< 0.05	< 0.05				
Yb	< 0.05	< 0.05	< 0.05	< 0.05				
Lu	< 0.05	< 0.05	< 0.05	< 0.05				
Hf	< 0.05	< 0.05	< 0.05	< 0.05				
Ta	< 5	< 5	< 5	< 5				
W	0.11	< 0.05	0.35	0.7				
Re	< 0.05	< 0.05	< 0.05	< 0.05				
Os	< 0.05	< 0.05	< 0.05	< 0.05				
Ir	< 0.05	< 0.05	< 0.05	< 0.05				
Pt	< 0.05	< 0.05	< 0.05	< 0.05				
Au	< 0.1	< 0.1	< 0.1	< 0.1				
Hg	< 0.5	< 0.5	< 0.5	< 0.5				
T1	< 0.1	< 0.1	< 0.1	< 0.1				
Pb	< 0.5	< 0.5	< 0.5	< 0.5				
Bi	< 0.1	< 0.1	< 0.1	< 0.1				
Th	< 0.05	< 0.05	< 0.05	< 0.05				
U	< 0.05	< 0.05	< 0.05	< 0.05				

Table 6-2. Impurity analysis report for heat-treated compact A3-P33-Z10



**GDMS** ANALYTICAL REPORT SHIVA Technologies An Operating Unit of Evans Analytical Group LLC 6707 Brooklawn Parkway Syracuse, New York 13211

Telephone (315) 431-9900 Fax: (315) 431-9800 Email info.ny@eaglabs.com www.eaglabs.com

Customer: **UT-Battelle Oak Ridge**  P.O.#

4000100480

1 Bethel Valley Rd, Oak Ridge, TN 37823-6063 USA Date: 7-Nov-10

Job#

S0ABV776

Customer ID: C

Sample ID:

S101101069

A3-P33-Z10

Element	Concentration [ ppm wt ]	Element Concentratio [ ppm wt ]		
Li	< 0.01	Pd	< 0.1	
Be	< 0.01	Ag	< 0.1	
В	0.12	Cd	< 0.1	
С	Matrix	In	< 0.1	
N	-	Sn	< 0.5	
0	-	Sb	< 0.5	
F	< 1	Te	< 0.1	
Na	< 0.05		< 0.1	
Mg	6.2	Cs	< 0.1	
Al	22	Ва	< 0.1	
Si	410	La	< 0.5	
Р	1	Ce	< 0.05	
S	26	Pr	< 0.05	
CI	0.18	Nd	< 0.05	
K	< 0.1	Sm	< 0.05	
Ca	16	Eu	< 0.05	
Sc	< 0.05	Gd	< 0.05	
Ti	0.51	Tb	< 0.05	
V	0.36	Dy	< 0.05	
Cr	< 0.5	Но	< 0.05	
Mn	< 0.05	Er	< 0.05	
Fe	0.05	Tm	< 0.05	
Со	< 0.05	Yb	< 0.05	
Ni	< 0.1	Lu	< 0.05	
Cu	< 0.1	Hf	< 0.05	
Zn	< 0.1	Та	< 5	
Ga	< 0.1	W	0.11	
Ge	< 0.1	Re	< 0.05	
As	< 0.1	Os	< 0.05	
Se	< 0.1	lr	< 0.05	
Br	< 0.1	Pt	< 0.05	
Rb	< 0.05	Au	< 0.1	
Sr	< 0.05	Hg	< 0.5	
Υ	< 0.05	ΤΪ	< 0.1	
Zr	0.5	Pb	< 0.5	
Nb	< 0.1	Bi	< 0.1	
Мо	0.11	Th	< 0.05	
Ru	< 0.1	U	< 0.05	
Rh	< 0.1			

J.SCHIEBLER (Analyst)

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Table 6-3. Impurity analysis report for heat-treated compact A3-P33-Z13



GDMS
ANALYTICAL REPORT

SHIVA Technologies An Operating Unit of Evans Analytical Group LLC 6707 Brooklawn Parkway Syracuse, New York 13211 Telephone (315) 431-9900 Fax: (315) 431-9800 Email info.ny@eaglabs.com www.eaglabs.com

Customer: UT-Battelle Oak Ridge

P.O.#

4000100480

1 Bethel Valley Rd, Oak Ridge, TN 37823-6063 USA 7-Nov-10

Job#

S0ABV776

Customer ID: C

Sample ID:

S101101070

A3-P33-Z13

Element	Concentration [ ppm wt ]	Element Concentration [ ppm wt ]		
Li	< 0.01	Pd	< 0.1	
Be	< 0.01	Ag	< 0.1	
В	0.06	Cd	< 0.1	
С	Matrix	In	< 0.1	
N	-	Sn	< 0.5	
0	-	Sb	< 0.5	
F	< 1	Те	< 0.1	
Na	< 0.05	I	< 0.1	
Mg	3.2	Cs	< 0.1	
Al	14	Ва	< 0.1	
Si	330	La	< 0.5	
Р	0.66	Ce	< 0.05	
S	25	Pr	< 0.05	
Cl	0.07	Nd	< 0.05	
K	< 0.1	Sm	< 0.05	
Ca	17	Eu	< 0.05	
Sc	< 0.05	Gd	< 0.05	
Ti	0.31	Tb	< 0.05	
V	0.22	Dy	< 0.05	
Cr	< 0.5	Но	< 0.05	
Mn	< 0.05	Er	< 0.05	
Fe	0.08	Tm	< 0.05	
Со	< 0.05	Yb	< 0.05	
Ni	< 0.1	Lu	< 0.05	
Cu	< 0.1	Hf	< 0.05	
Zn	< 0.1	Та	< 5	
Ga	< 0.1	W	< 0.05	
Ge	< 0.1	Re	< 0.05	
As	< 0.1	Os	< 0.05	
Se	< 0.1	Ir	< 0.05	
Br	< 0.1	Pt	< 0.05	
Rb	< 0.05	Au	< 0.1	
Sr	< 0.05	Hg	< 0.5	
Υ	< 0.05	TI	< 0.1	
Zr	0.22	Pb	< 0.5	
Nb	< 0.1	Bi	< 0.1	
Мо	0.1	Th	< 0.05	
Ru	< 0.1	U	< 0.05	
Rh	< 0.1			

J.SCHIEBLER (Analyst)

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Table 6-4. Impurity analysis report for heat-treated compact A3-P33-Z17



GDMS
ANALYTICAL REPORT

SHIVA Technologies An Operating Unit of Evans Analytical Group LLC 6707 Brooklawn Parkway Syracuse, New York 13211 Telephone (315) 431-9900 Fax: (315) 431-9800 Email info.ny@eaglabs.com www.eaglabs.com

Customer: UT-Battelle Oak Ridge

P.O.#

4000100480

1 Bethel Valley Rd, Oak Ridge, TN 37823-6063 USA Date: 8-Nov-10

Job #

S0ABV776

Customer ID: C

Sample ID:

S101101071

A3-P33-Z17

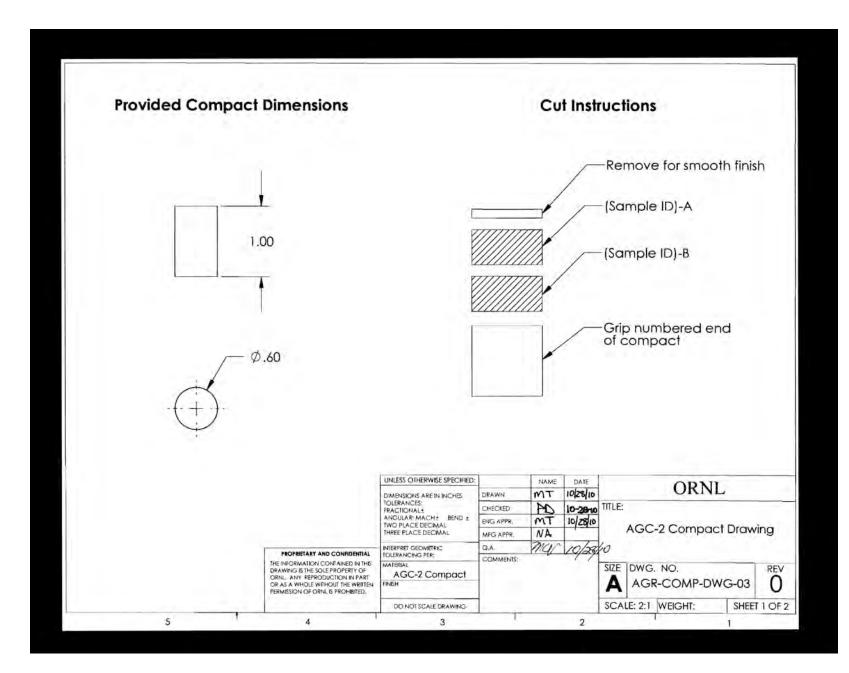
Element	Concentration [ ppm wt ]	Element	Concentration [ ppm wt ]	
Li	< 0.01	Pd	< 0.1	
Be	< 0.01	Ag	< 0.1	
В	0.12	Cd	< 0.1	
С	Matrix	In	< 0.1	
N	-	Sn	< 0.5	
0	_	Sb	< 0.5	
F	< 1	Te	< 0.1	
Na	< 0.05		< 0.1	
Mg	12	Cs	< 0.1	
Al	31	Ba	0.34	
Si	540	La	< 0.5	
P	1.3	Ce	< 0.05	
S	47	Pr	< 0.05	
CI	0.44	Nd	< 0.05	
K	< 0.1	Sm	< 0.05	
Ca	110	Eu	< 0.05	
Sc	< 0.05	Gd	< 0.05	
Ti	2.7	Tb	< 0.05	
V	1.7	Dv	< 0.05	
Cr	< 0.5	Ho	< 0.05	
Mn	< 0.05	Er	< 0.05	
Fe	0.09	Tm	< 0.05	
Со	< 0.05	Yb	< 0.05	
Ni	< 0.1	Lu	< 0.05	
Cu	< 0.1	Hf	< 0.05	
Zn	< 0.1	Та	< 5	
Ga	< 0.1	W	0.35	
Ge	< 0.1	Re	< 0.05	
As	< 0.1	Os	< 0.05	
Se	< 0.1	lr	< 0.05	
Br	< 0.1	Pt	< 0.05	
Rb	< 0.05	Au	< 0.1	
Sr	0.08	Hg	< 0.5	
Y	0.13	TÏ	< 0.1	
Zr	1.9	Pb	< 0.5	
Nb	< 0.1	Bi	< 0.1	
Mo	0.25	Th	< 0.05	
Ru	< 0.1	Ü	< 0.05	
Rh	< 0.1			

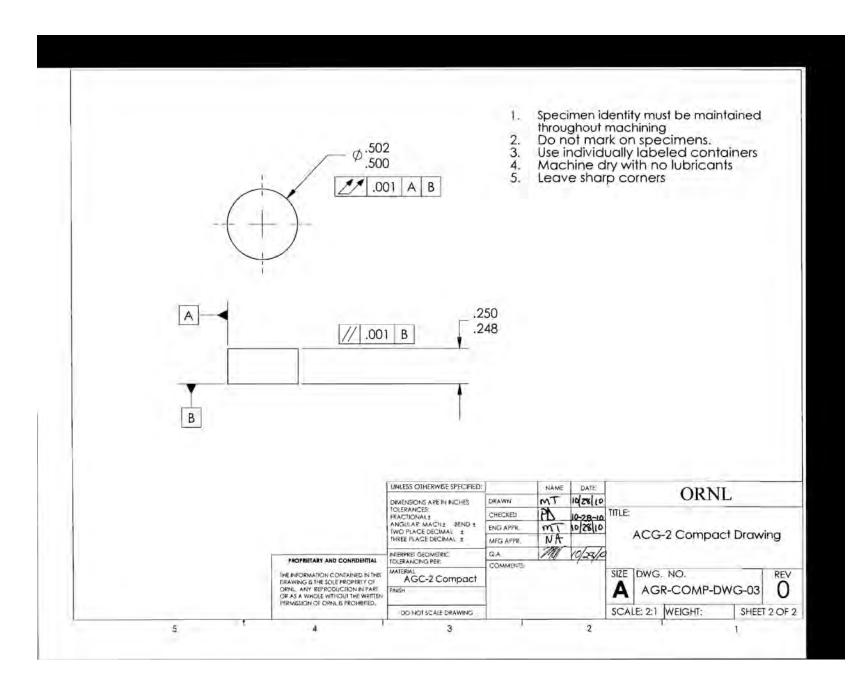
J.SCHIEBLER (Analyst)

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# **Appendix A: Compact Machining Drawings**

Prior to heat-treatment, carbonized cylinders were machined according to drawing AGR-COMP-DWG-03, "AGC Compact Drawing". Copies of these drawings are attached in this appendix.





### **Appendix B: Certificate of Conformance**

This section contains the Certificate of Conformance for the A3-P33 compact lot. This is a record of the review by Quality Assurance personnel that specified requirements in INL SPC-1285, Rev. 1 have been met. All compacts selected for irradiation or impurity analysis met all dimensional and density specifications. Note that the specification only requires compacts used for irradiation meet these requirements, so the final determination of this inspection is that the product (compacts used for irradiation) conforms to the specified requirements for length, diameter, and density.

Page 1 of 1

# Oak Ridge National Laboratory Advanced Gas Reactor Fuel Development and Qualification Program CERTIFICATE OF CONFORMANCE

1. ITEM IDENTIFICATION: AGC-2 Matrix-only Compacts									
	2. PART LOT AND LOT NUMBER: INL Blend E with Plenco 14433, Lot A3-P33								
3. PRODUCT DEFINITION: INL SPC-1285, Revision 1, Matrix Compacts for AGC-2 Irradiation 4. LIST OF APPROVED DEVIATIONS: Not Applicable									
						Liniana Dant	OTV	INUT	Data
*Part Type	Unique Part I.D. No.	QTY	INIT.	Date	*Part Type	Unique Part I.D. No.	QTY	INIT.	Date
MC	A3-P33-Z09	1	MOV	Illulio					
MC	A3-P33-Z20	1	mu	While					
MC	A3-P33-Z18	1	MIN	11/11/10					
			1.0	1					
		-							
-				-			-		
		- 17		-			-	-	
									-
	OF INDIVICE	DI DIVIG	VACANTES	DIELING	DDDCT				
5. LIST	OF APPLICA	BLE NO	NCONFO	RMANCE	REPOR	T NUMBERS:	Not App	licable	
With the		- Davist	d		Comeson or				
						referenced in Ite in Item 5, the lis			orming
						AP for the AGR			
						ing procedures,			product
	n prescribed in					ing procedures,	and to the	specifica p	roduct
35552181175	· Nacordopaga in 190	THE VEGET SE		- 20-3 50-121					
7	ny							1.1	
//	1.4	.0	1 - 0 - 0				-4	/11/	10_
M. C. Vance, AGR Quality Representative,  Date									

Fuel Cycle and Isotopes Division, ORNL

<sup>\*</sup> MC indicates matrix-only compact